



**MS&T2012: “Solidification, Crystal Growth and
Microstructural Correlation with Properties of Materials: To
Celebrate 75th Birthday of Prof. Martin E. Glicksman “**

Morphology of Primary-Dendrite Array: Observations from Ground-based and Space Station Processed Samples

Surendra N. Tewari – Cleveland State University

Ravi S. Rajamure – Cleveland State University*

Richard N. Grugel – Marshall Space Flight Center

Robert E. Erdman – The University of Arizona

David R. Poirier – The University of Arizona

This Investigation is a Collaborative Effort with the European Space Agency (ESA) Program MICAST

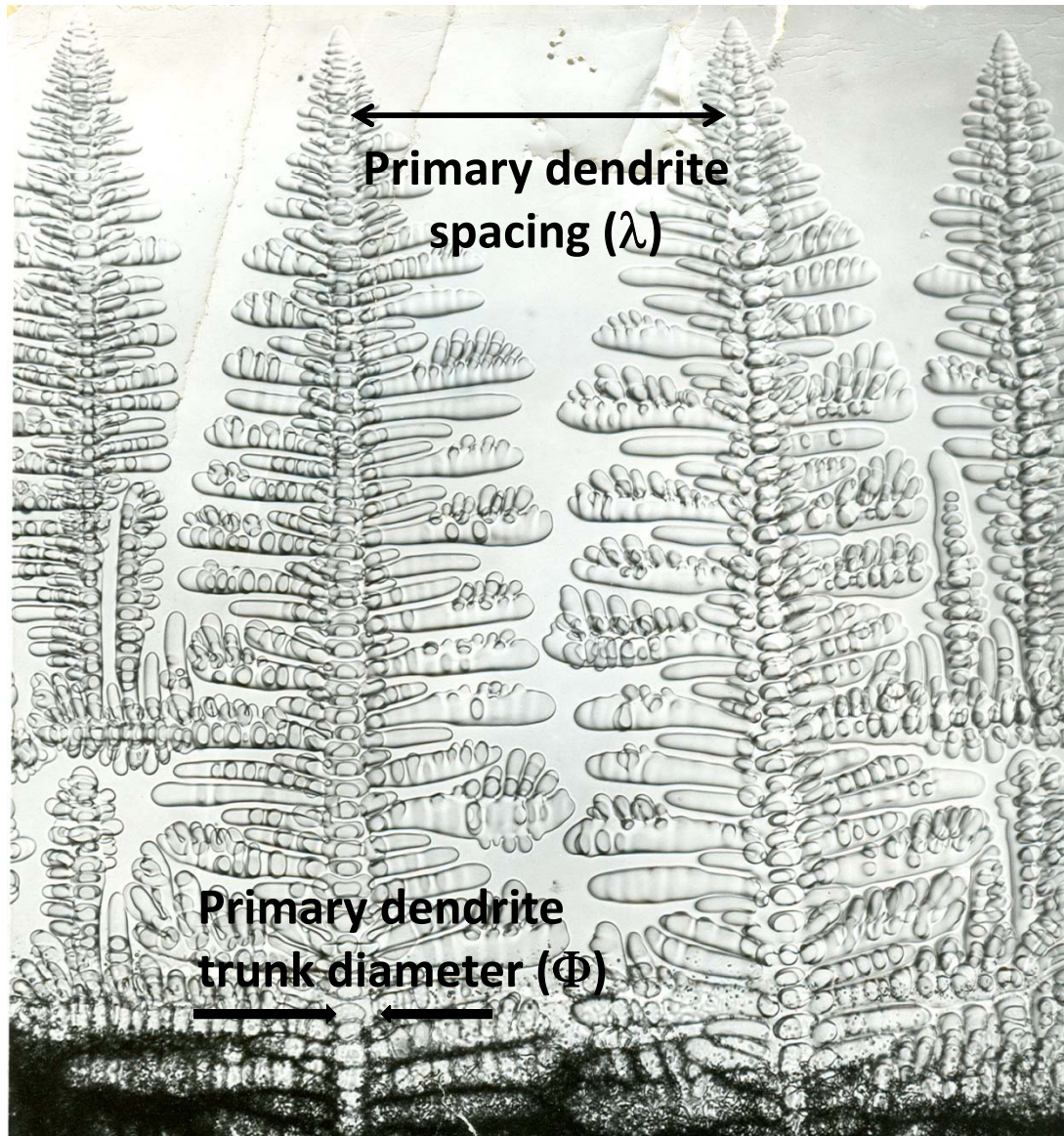
(Microstructure Formation in Castings of Technical Alloys under Diffusive and Magnetically Controlled Convective Conditions)

MICAST Purpose: A systematic analysis of the effect of convection on the microstructural evolution in cast binary, ternary and commercial Al-Si based alloys.

This research (MICAST6 and MICAST 7): DS dendritic mono-crystals of Al-7% Si (9-mm dia, 25 cm long) in μg .

Advantages:	Minimize Thermo-Solutal Convection
Intent:	Produce Segregation Free Samples Grown Under Diffusion-Controlled Conditions
Purpose:	Better Understand the Relationship between Processing and Microstructure-Development

Dendritic array morphology depends upon DS processing parameters: G_I , R , C_o , *Convection*



1. Primary dendrite arm spacing (λ): Extensive literature (SCN/Metals)
2. Secondary/tertiary arm spacing: Extensive-SCN/Metals
3. Dendrite tip radius: SCN/limited (Al-Cu, Pb-Au, Pb-Pd)
4. Primary dendrite trunk diameter (Φ): Limited (Esaka:Thesis-86, Grugel: 92/95)

Microgravity Processing : Partially remelt and then DS from terrestrially grown dendritic mono-crystal in μg .



(Al-7%Si Single Crystal Dendritic)



ESA- Sample Cartridge Assembly

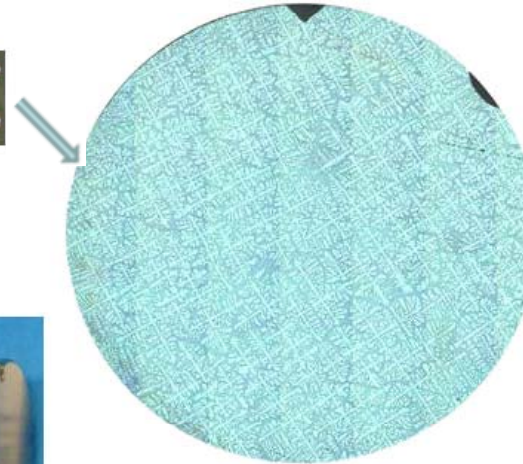


ESA_MSL Low Gradient Furnace



ESA:
Material
Science
Laboratory

NASA_MSSR-1 Flight Rack



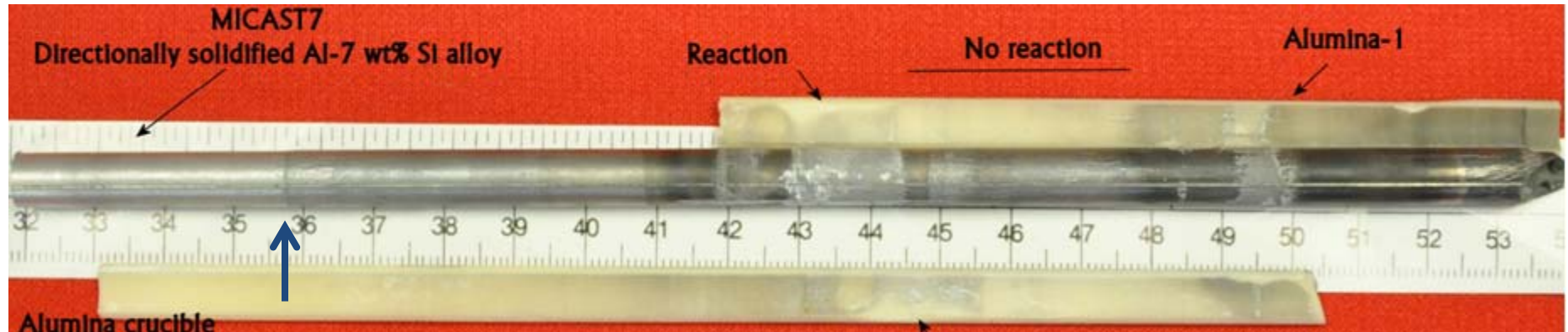
Transverse View

Microgravity Processed Sample MICAST 7



Eutectic Melt Back
/ Isotherm

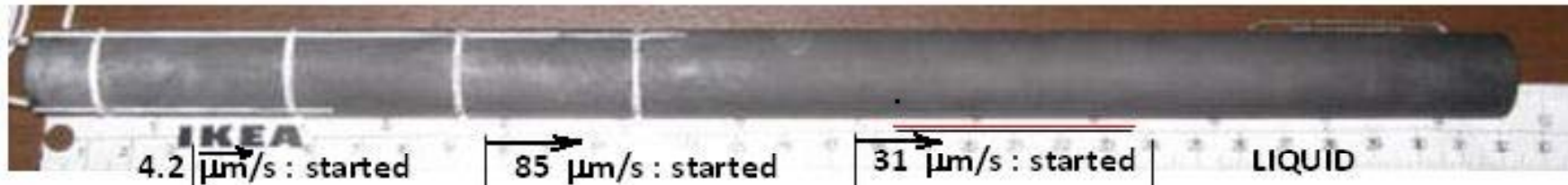
X-ray radiograph of MICAST7



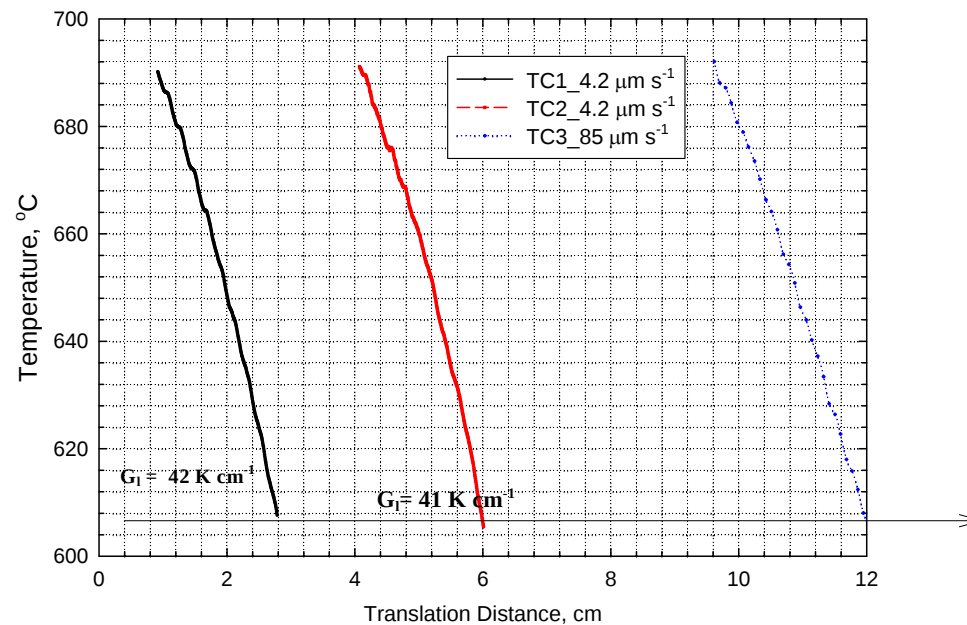
Eutectic Melt Back

Terrestrial processing

Graphite crucible (~9 mm ID, ~19 mm OD), 10^{-4} torr vacuum



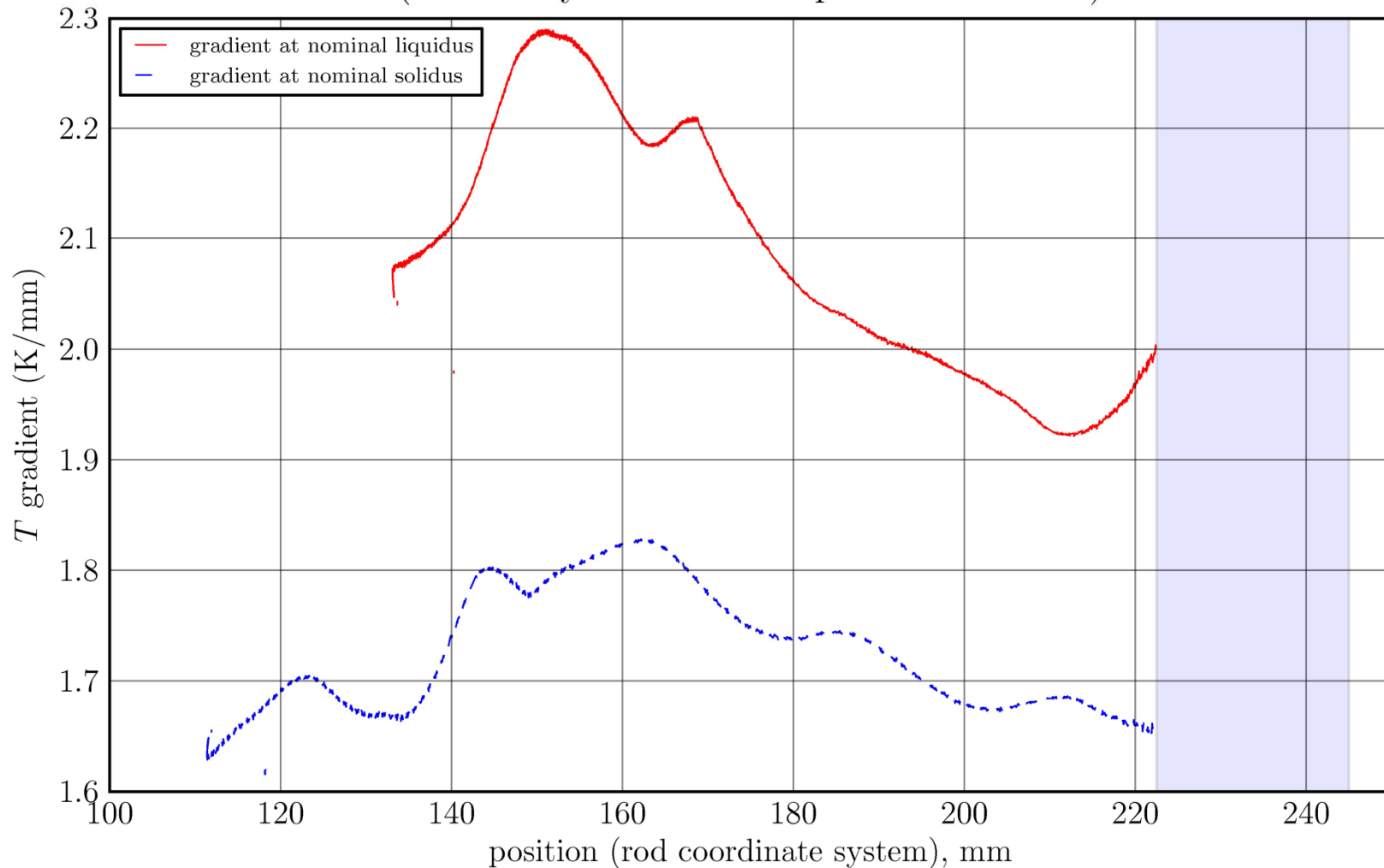
Thermal Gradient at the liquidus temperature
(Al-7%Si, Graphite Crucible, 3 TCs located along crucible length)



Don't have terrestrial samples which are processed in LGF or LGFQ equivalent hardware under R and G_1 conditions which are identical to MICAST6, MICAST7

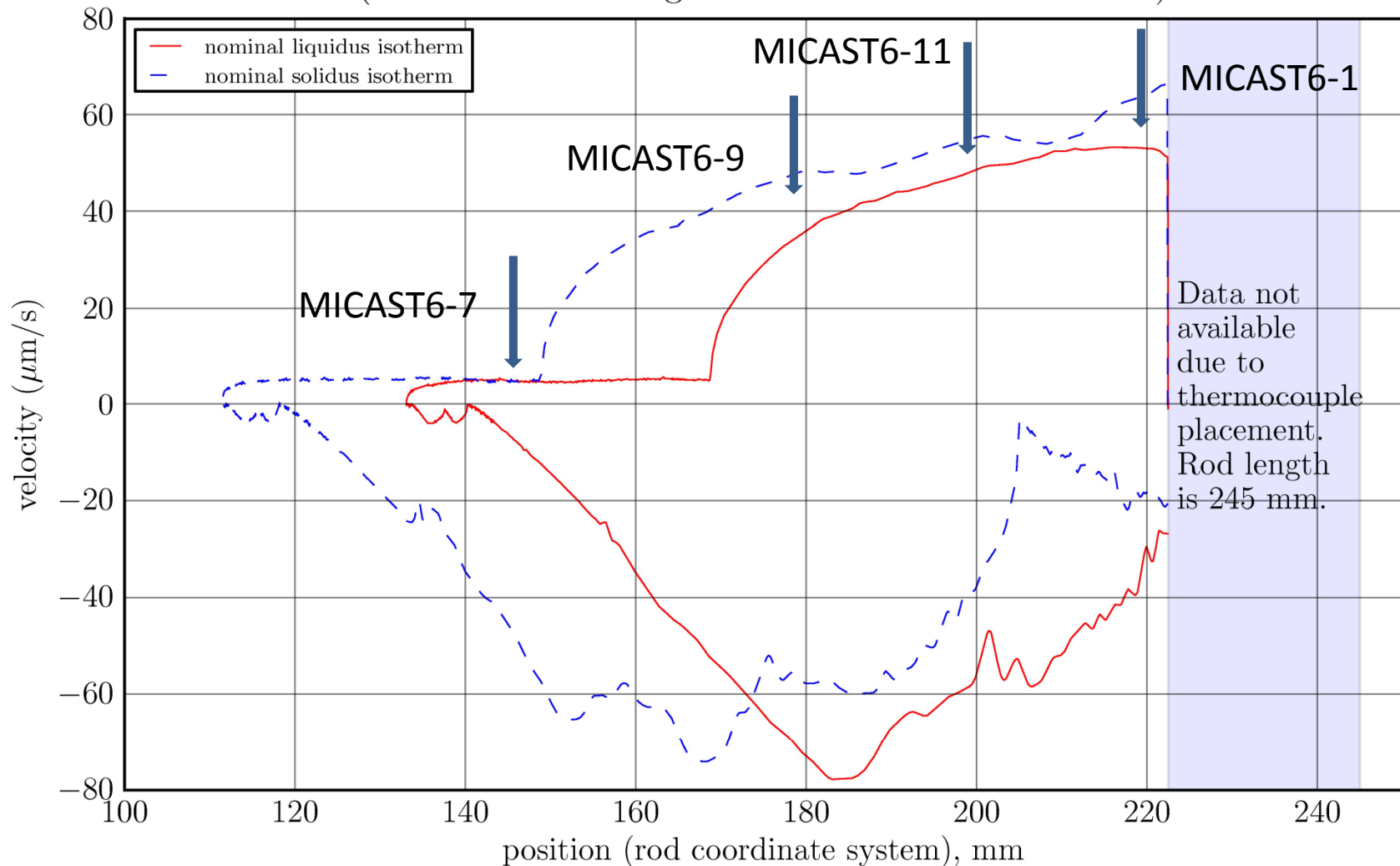
MICAST6: ESA-Low Gradient Furnace (1-hr heat-up, 5-hr hold, $G_l \sim 20 \text{ K cm}^{-1}$): 3.8 cm at $5 \mu\text{m s}^{-1}$, 11.3 cm at $50 \mu\text{m s}^{-1}$

temperature gradients at nominal liquidus and solidus isotherms
(note: only solidification portion is shown)



MICAST6: ESA-Low Gradient Furnace (1-hr heat-up, 5-hr hold, $G_1 \sim 20 \text{ K cm}^{-1}$): 3.8 cm at $5 \mu\text{m s}^{-1}$, 11.3 cm at $50 \mu\text{m s}^{-1}$

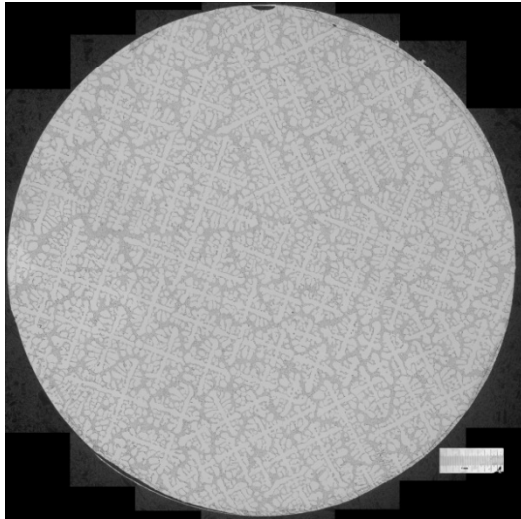
isotherm velocity vs. position along the Al-Si rod
(note: both melting and solidification are shown)



Comparison of microstructures: Al-7% Si directionally solidified on ground and on ISS (MICAST6)

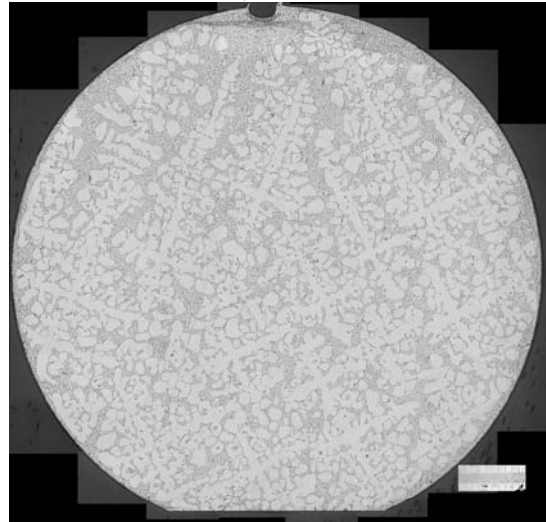
MICAST6 SEED

41 K cm^{-1} , $22 \mu\text{m s}^{-1}$

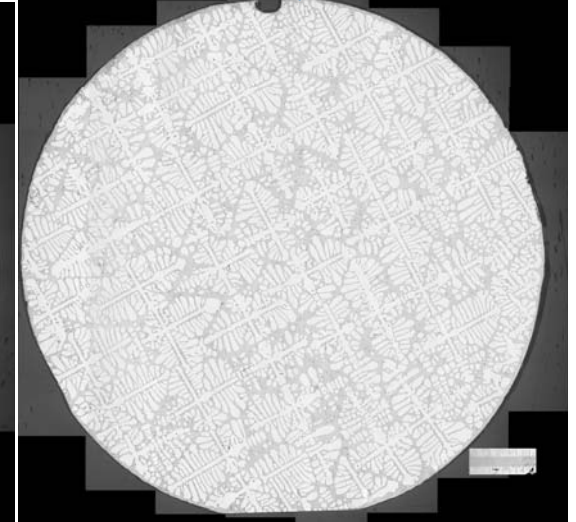


MICAST6: 20 K cm^{-1}

$5 \mu\text{m s}^{-1}$



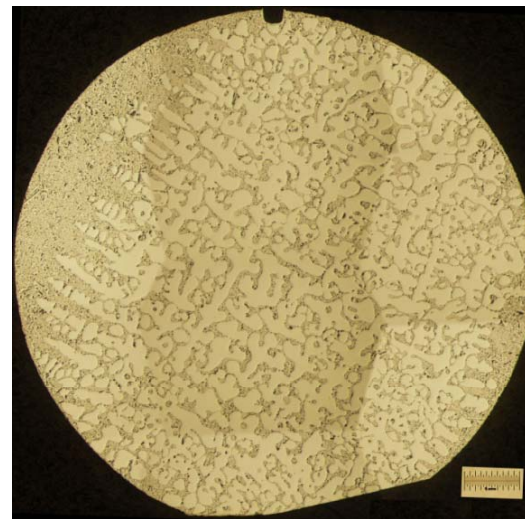
$50 \mu\text{m s}^{-1}$



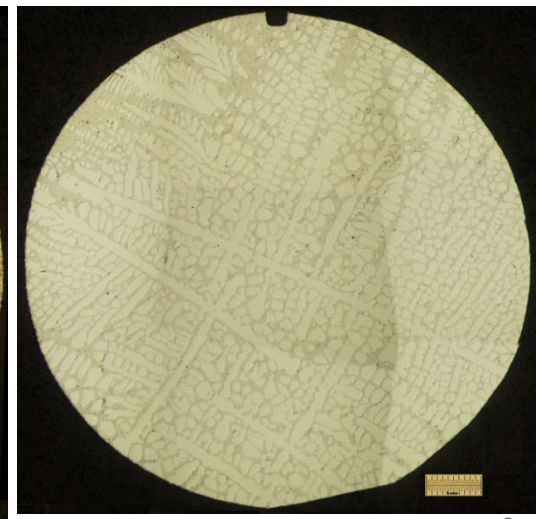
Terrestrial DS:

15 K cm^{-1} →

Convection causes dendrite clustering (steeping) at low thermal gradient and growth speeds during terrestrial DS.

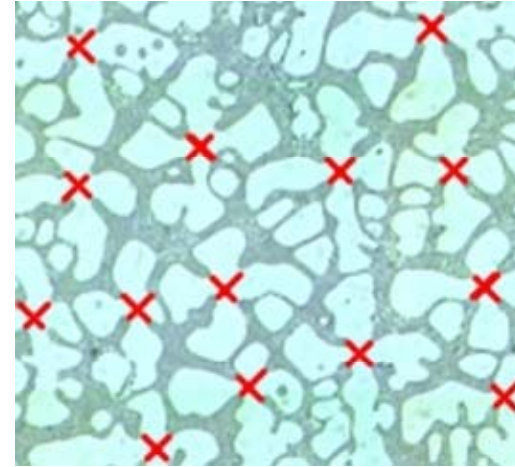
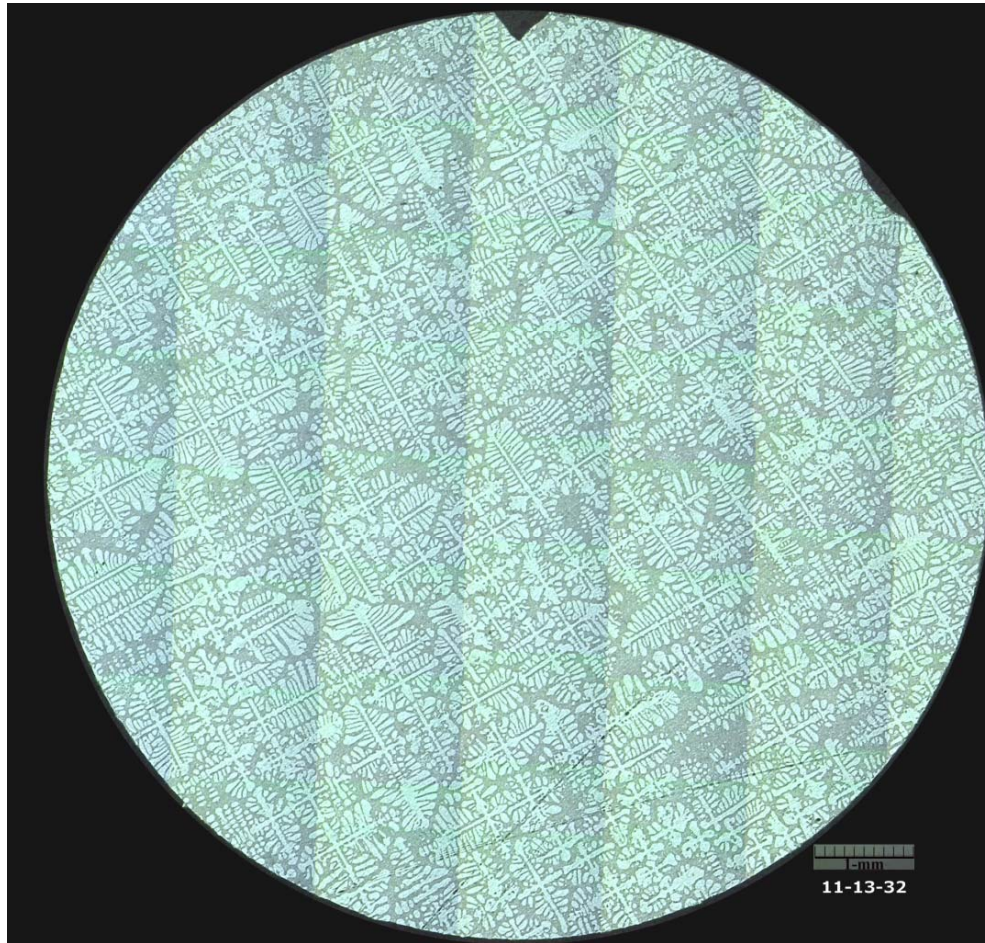


$5 \mu\text{m s}^{-1}$

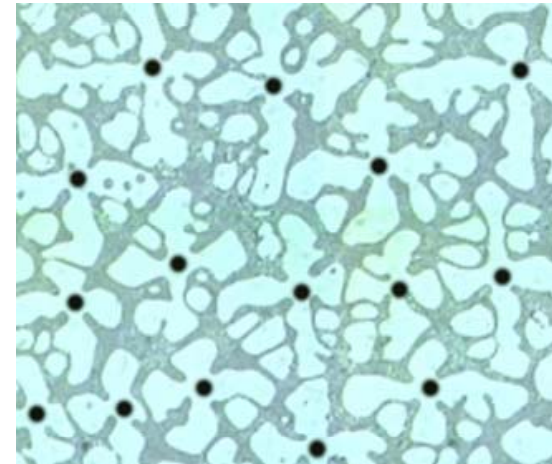


$50 \mu\text{m s}^{-1}$

Typical analysis of directionally solidified Al-7 wt% Si alloy samples (Terrestrial: $G_l=41 \text{ Kcm}^{-1}$, $R=85 \text{ } \mu\text{m s}^{-1}$, $G_m=51 \text{ K cm}^{-1}$)

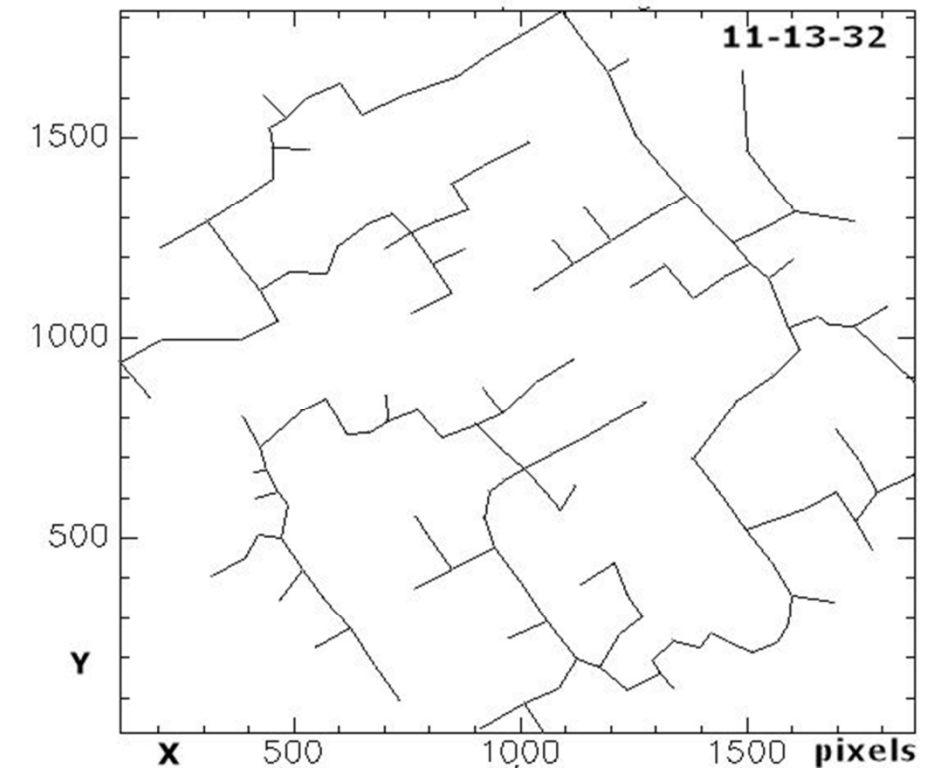
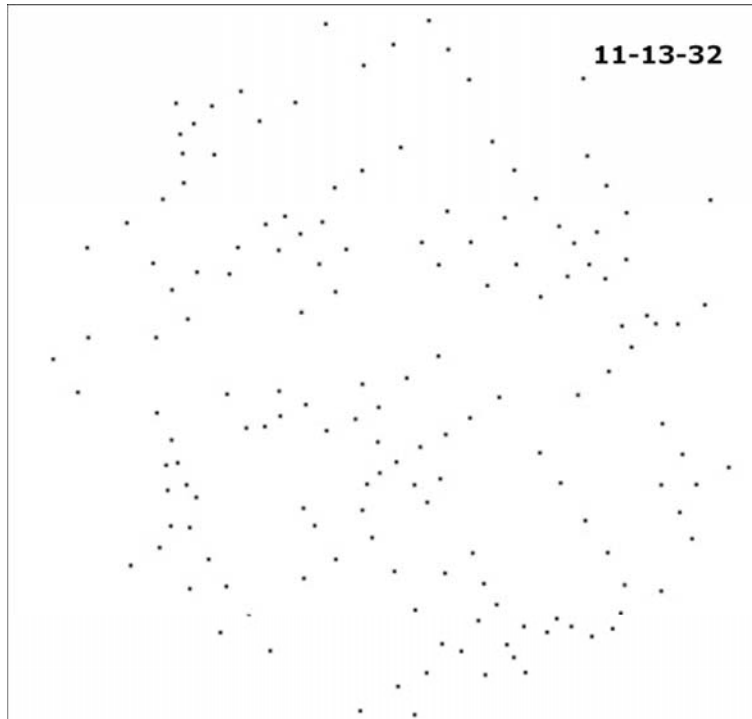


Primary dendrite trunk diameter



Primary dendrite arm spacing???

Which primary dendrite arm spacing to use?



Primary spacing $\sqrt{A/(N-1)} = 623 \mu\text{m}$

MST spacing = $412 \pm 138 \mu\text{m}$

Nearest neighbor spacing = $368 \pm 126 \mu\text{m}$

Primary spacing by $\sqrt{A/(N-1)}$ method is 1.69 times the nearest neighbor spacing → Theoretical models predict *nearest neighbor spacing*

Theoretical models for primary dendrite arm spacing

$$(m_l G_c^t - G_t) / (4\pi^2 \Gamma T_m / r_t^2) = 1 \text{ for small } R r_t / 2D_l$$

$$r_t = - \frac{G_L \lambda_1^2}{4\sqrt{2} [m_L C_t (1-k) + \frac{D_L G_L}{R}]}$$

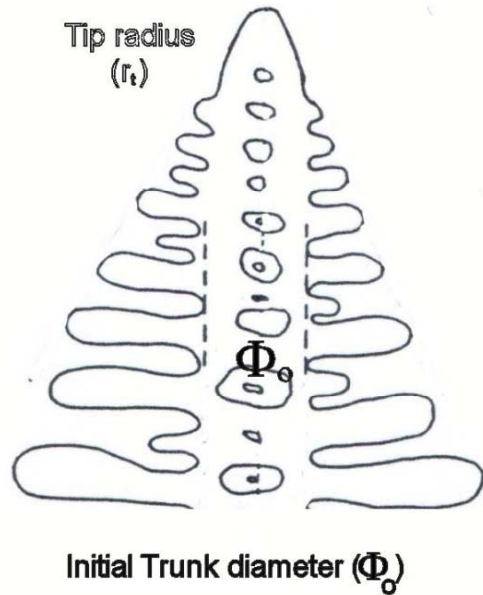
	<u>Analytical</u>	<u>Numerical</u>
Tip radius:	Trivedi (1980)	Hunt-Lu (1996)
Primary spacing:	Trivedi (1984)	Hunt- Lu (1996)
Trunk diameter:	None	

Physical Properties for Al- 7 wt% Si

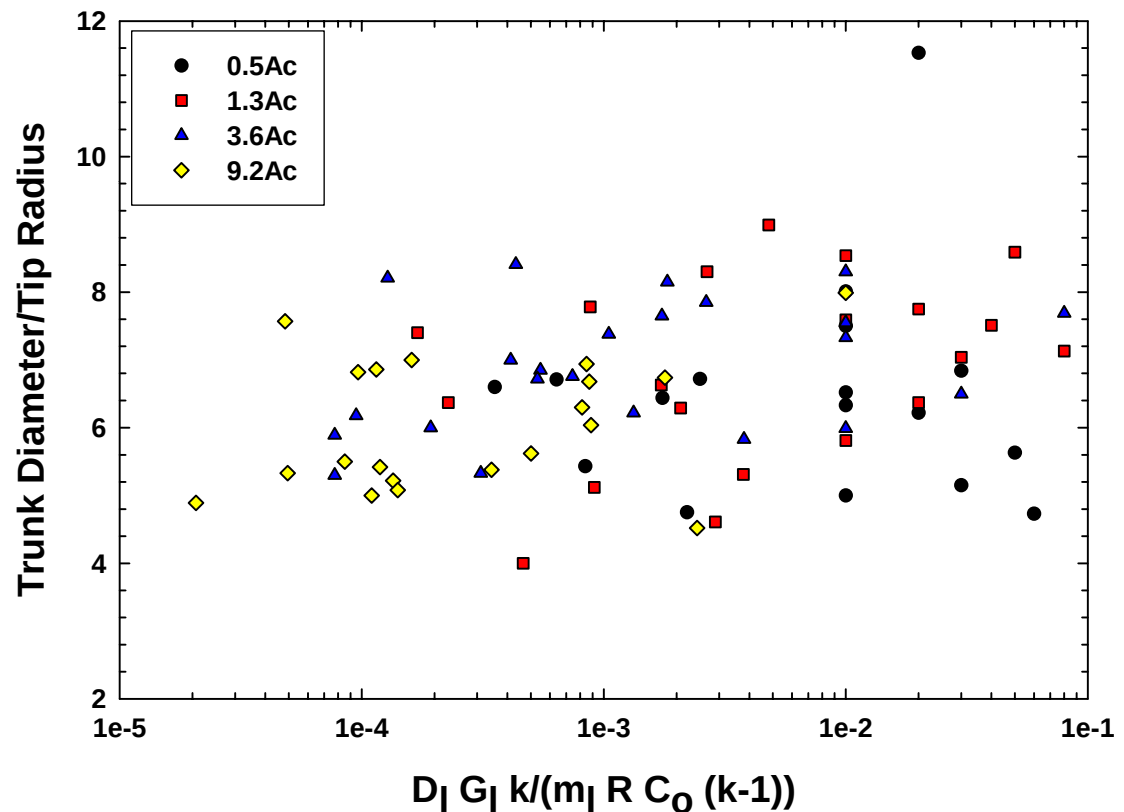
Co	7 wt% Si	
m_l	-6.31 K/ wt% Si	Metals Handbook, vol 8(1973)
k	0.1	
Γ	0.196 $\mu\text{m K}$	Gunduz and Hunt (1985)
D_l	$4.3 \times 10^{-9} \text{ m}^2/\text{s}$	(Poirier compilation)

Primary dendrite trunk diameter (ϕ)

Esaka Thesis (1986): Trunk diameter increases rapidly near the tip till ~ 10 side-branch formations. He measured this **initial trunk diameter (ϕ_o)**. Eighty DS experiments (four SCN-Acetone alloys grown with various R and G_I)



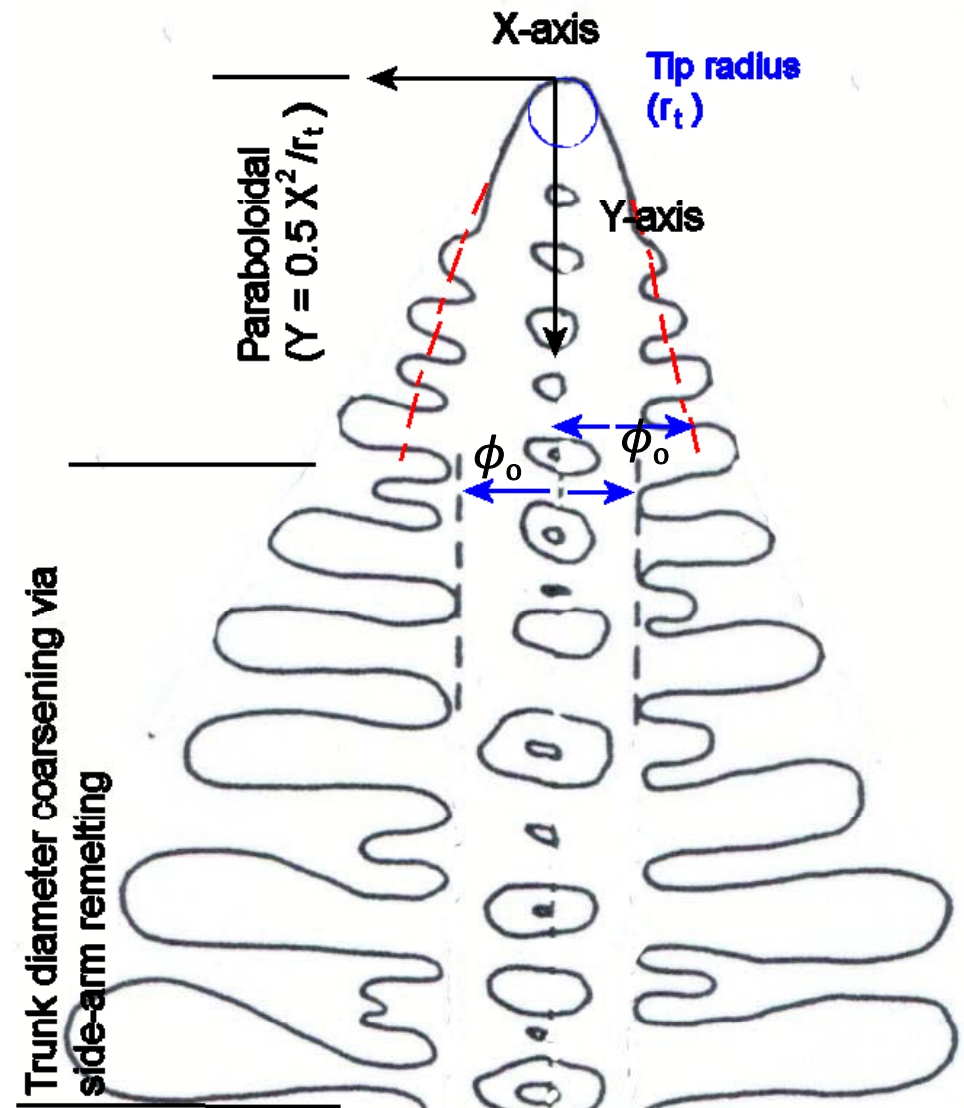
$D_I G_I k / (m_I R C_o (k-1))$]: More branched dendritic morphologies will be located towards the left, and less-branched/cellular towards the right side of the X-axis.



$$(\text{Initial trunk diameter } (\phi_o) / \text{tip radius}) = 6.59 \pm 1.3$$

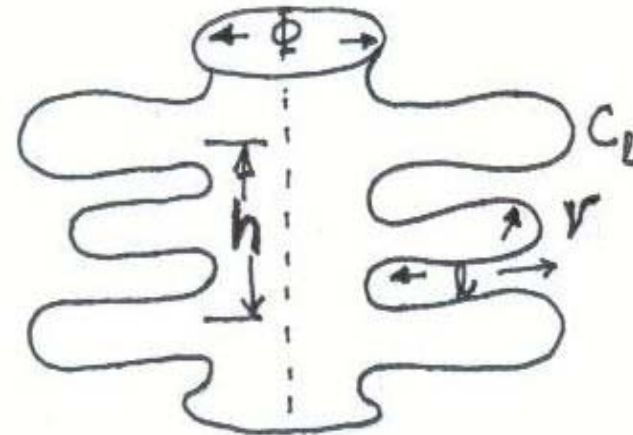
Primary dendrite trunk diameter (ϕ) model

1. The trunk diameter (ϕ) increases rapidly near the tip till time, $t_o = 22 * r_t / R$, when $\phi = \phi_o = 6.59 r_t$ (paraboloidal envelope near tip).



Primary dendrite trunk diameter (ϕ) model

- After t_0 the trunk diameter increases via remelting of 4-side arms (r) and deposition of melted arm material on “trunk surface “over length h ” = ϕ .



Assumptions:

- Kirkwood model (1985) of ripening applies.
- Secondary arm melts back because of its curvature.
- Mass of the melted arm deposits on trunk surface where there is negative curvature.

$$\frac{dl}{dt} = \frac{4 D_l \Gamma}{m_l C_l (1-k) r^2} \quad (1)$$

$$\pi \phi h \frac{d\phi}{2 dt} = 4 * \pi r^2 \frac{dl}{dt} \quad (2)$$

$$C_l = C_o + R G_m t / m_l \quad (3)$$

$$\phi^2 \frac{d\phi}{dt} = 32 \frac{D_l \Gamma}{m_l (1-k) (C_o + \frac{R G_m t}{m_l})} \quad (4)$$

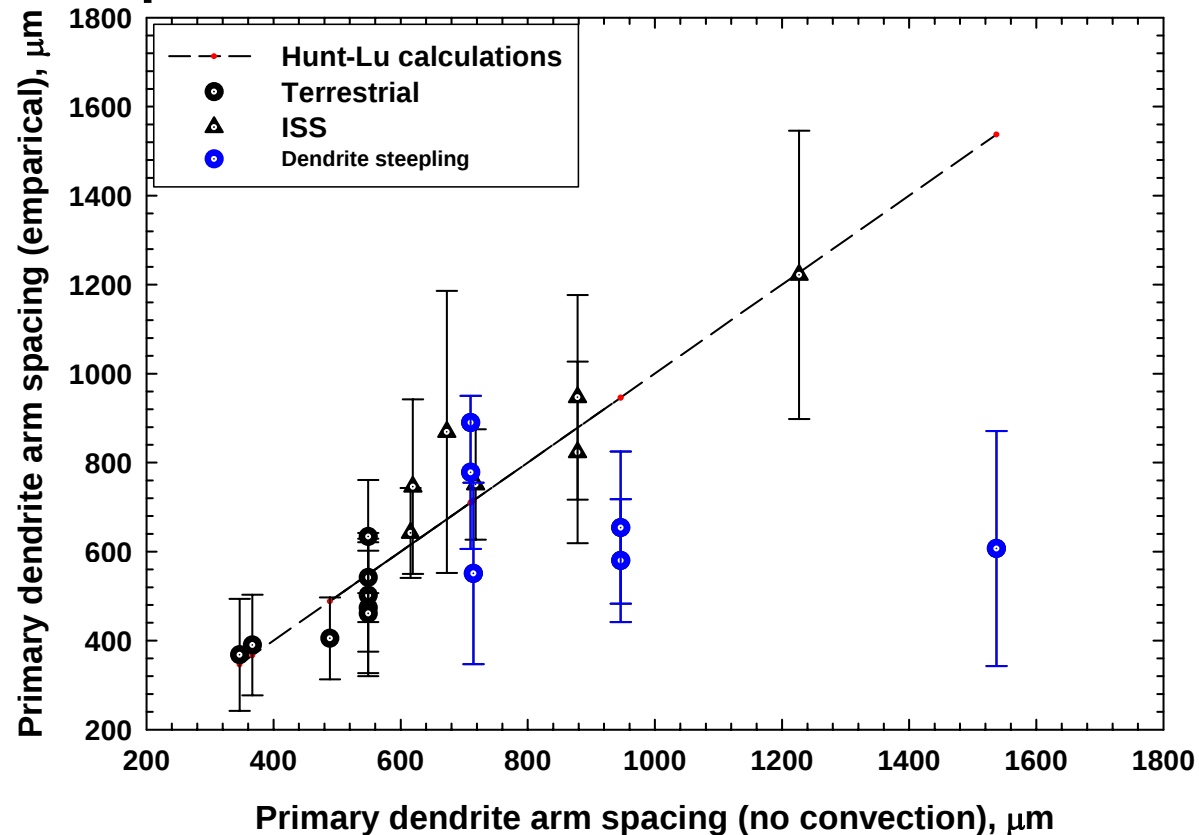
Primary dendrite trunk diameter (ϕ) model

$$\phi^3 = 96 \frac{D_l \Gamma}{R G m (1 - k)} \ln \left\{ \frac{\left(1 + \frac{R G m t}{m_l C_o} \right)}{\left(1 + \frac{R G m t_o}{m_l C_o} \right)} \right\} + \Phi_o^3$$

Mushy zone freezing time $\sim m_l(C_E - C_o)/R G_m$

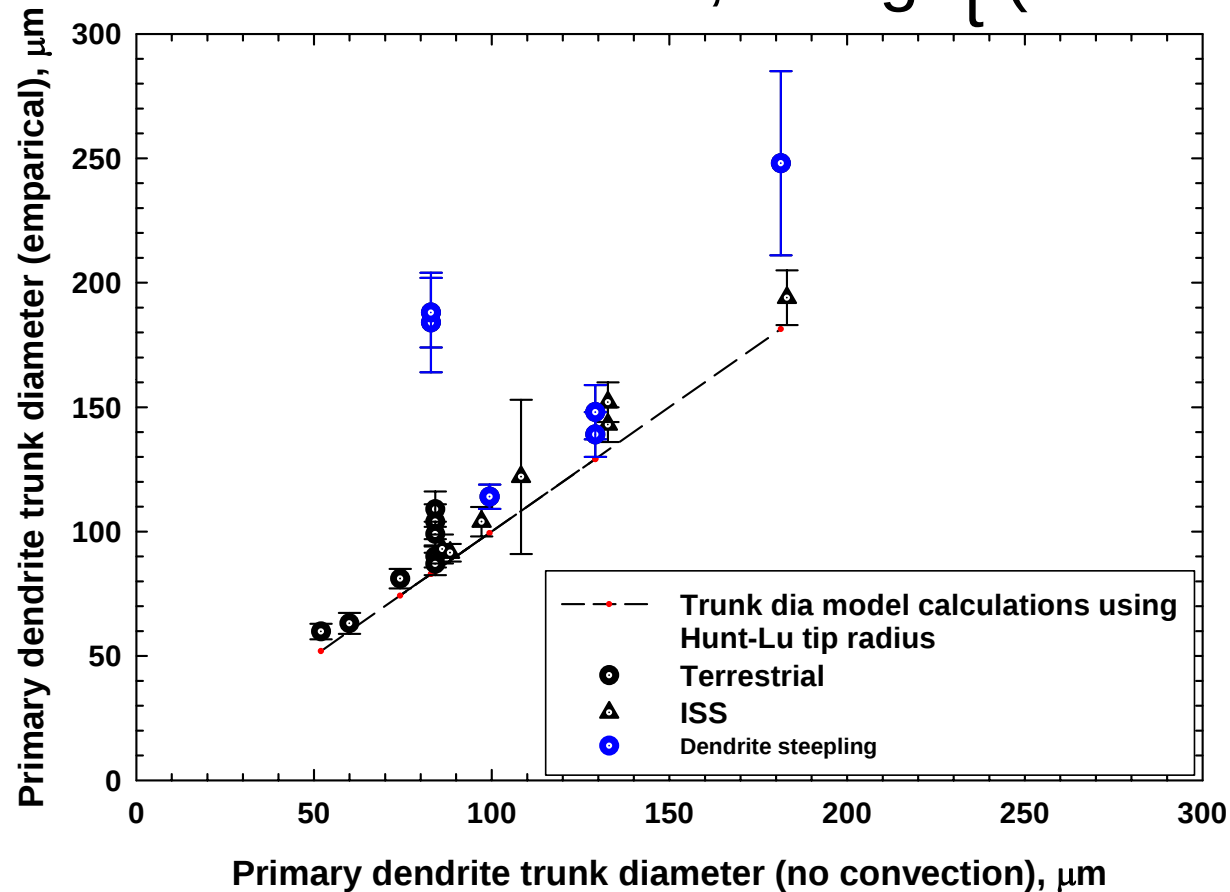
Use tip radius (r_t) predicted from Trivedi (1980) or Hunt-Lu (1996) models to get the initial trunk diameter $\phi_o = 6.59 r_t$ in order to predict the processing parameter dependence of “Primary dendrite trunk diameter” from above relationship.

Primary dendrite arm spacings as compared to Hunt-Lu calculations



- ISS-DS: Good agreement with predictions from Hunt-Lu model.
- Terrestrial DS ("Not steepled") : Good agreement with predictions from Hunt-Lu model.
- Terrestrial DS ("steepled"): Convection decreases primary dendrite arm spacing.

Primary dendrite trunk diameter as compared to trunk diameter model calculations, using r_t (Hunt-Lu)



- ISS-DS: Good agreement with predictions from the trunk-diameter model.
- Terrestrial DS ("Not steeped") : Good agreement with predictions from model.
- Terrestrial DS ("steeped"): Convection increases trunk diameter.

Conclusions

- Primary dendrite arm spacings of Al-7 wt% Si alloy directionally solidified in low gravity environment of space (MICAST-6 and MICAST-7: Thermal gradient ~ 19 to 26 K cm^{-1} , Growth speeds varying from 5 to $50 \mu\text{m s}^{-1}$) show a good agreement with predictions from Hunt-Lu and Trivedi models.
- Primary dendrite trunk diameters of the ISS processed samples show a good fit with a simple analytical model based on Kirkwood's approach, proposed here.
- Natural convection,
 - decreases primary dendrite arm spacing.
 - appears to increase primary dendrite trunk diameter.

Acknowledgements

- NASA
- ESA
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